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## RESEARCH MEMORANDUM

for the

Bureau of Aeronautics, Navy Department

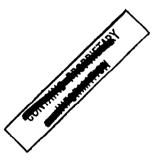
PRELIMINARY RESULTS OF ALTITUDE-WIND-TUNNEL INVESTIGATION

OF X24C-4B TURBOJET ENGINE

V - PERFORMANCE OF MODIFIED ENGINE

By William R. Prince, and Harry E. Bloomer

Flight Propulsion Research Laboratory Cleveland, Ohio



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# NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS

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#### SUMMARY

An investigation has been conducted in the NACA Cleveland altitude wind tunnel to evaluate the performance characteristics of a modified X24C-4B turbojet engine over a range of simulated altitudes from 5000 to 45,000 feet, simulated flight Mach numbers from 0.25 to 1.07, and engine speeds from 4000 to 12,500 rpm. The engine was modified by the manufacturer to improve the velocity and temperature profiles within the engine. Performance data are graphically presented to show the effect of altitude at a flight Mach number of 0.25 and the effect of flight Mach number at an altitude of 25,000 feet. Original and modified engine performances for several specific operating conditions are compared. A complete tabulation of average pressures and temperatures throughout the engine, performance data, and lubrication and fuel-system data is presented.

The average temperature pattern at the turbine outlet for the modified engine conformed more closely to the manufacturer's desired temperature distribution than for the original configuration. A comparison of original and modified engine performance data showed that with the modified configuration a thrust increase from 5 to 14 percent based on original engine output was obtained for several specific operating conditions. Application of the generalization factors showed that performance variables depending upon fuel consumption that are obtained at one altitude cannot be used in predicting the values of these parameters at any other altitude; however, thrust and air-flow values can be predicted for a limited range of altitudes from data taken at one altitude.



INTRODUCTION

Performance and operational characteristics of an X24C-4B turbojet engine have been investigated in the NACA Cleveland altitude wind tunnel at the request of the Bureau of Aeronautics, Navy Department. Data presenting pressure and temperature distributions, engine performance, and compressor performance are reported in references 1, 2, and 3, respectively.

A modified X24C-4B turbojet engine was investigated after completion of the tests of the original engine. Engine modifications were made by the manufacturer to improve the velocity and temperature profiles within the engine. The effect of the modifications on the compressor performance is presented in reference 4.

The effects of altitude and flight Mach number on the performance of the modified engine are presented herein. The applicability of methods used to generalize the data in order to estimate the performance at various altitudes from performance data obtained at any altitude is discussed. A complete tabulation of average pressures and temperatures throughout the engine, performance data, and lubrication and fuel-system data is presented.

#### APPARATUS AND INSTRUMENTATION

The modified engine was installed in a wing nacelle in the test section of the altitude wind tunnel in the same manner as the original engine (fig. 1). In order to obtain pressures at the engine inlet that corresponded to a wide range of flight Mach numbers, dry refrigerated air was supplied to the engine through a duct from the tunnel make-up air system. The compressor, the combustion chamber, and the exhaust nozzle of the basic X24C-4B engine, described in detail in reference 1, were modified for the present investigation.

The compressor was modified to improve the radial velocity distribution at the compressor-outlet annulus by twisting the eleventh-stage rotor blade tips 6° in the direction of reduced angle of attack.

The combustion chamber (fig. 2) was modified to improve the temperature distribution at the turbine inlet. The wall perforations of the fourth step of the combustion-chamber liner were omitted and the circular wall perforations in the third step were changed to rectangular. The total area of the holes in the third step of the modified liner was equal to the hole area of the third

and fourth steps in the original liner. Introducing the air into the combustion chamber farther upstream, and thereby increasing the penetration, improved the mixing in the secondary combustion zone. The blocking area of the screens at the annular combustion-chamber inlet was reduced. For the original configuration, a screen having 60-percent blocking area was installed in the outer annulus and one having 40-percent blocking area was installed in the intermediate annulus. In the modified combustion chamber, these screens were replaced by two screens of '30-percent blocking area. The fuel nozzles for the modified engine had a rated capacity of 7 gallons per hour at a differential pressure of 100 pounds per square inch, as compared to  $7\frac{1}{2}$  gallons per hour for the original engine.

With improved temperature distribution at the turbine inlet, the manufacturer increased the allowable temperature limits at the turbine outlet from 1250° to 1400° F, as indicated by the hottest thermocouple; a reduction in exhaust-nozzle area was consequently required to obtain the new temperature limits with the modified engine. The exhaust nozzle used in this investigation had an outlet area of 170.6 square inches as compared to an area of 183.1 square inches for the original engine.

Temperature and pressure measurements were obtained at eight stations in the engine (fig. 3). The instrumentation installed in the modified engine remained the same as that in the original configuration with the exception of the addition of three temperature rakes at the turbine outlet, making a total of 55 thermocouples at that survey station. Location and details of the instrumentation installed in the original engine are presented in reference 1.

#### PROCEDURE

Performance characteristics of the engine were obtained at simulated altitudes from 5000 to 45,000 feet, simulated flight Mach numbers from 0.09 to 1.07, and engine speeds from the idling speed of 4000 rpm to the rated speed of 12,500 rpm. For most operating conditions, the inlet-air temperature was held at approximately NACA standard values corresponding to the simulated flight conditions. Inlet-air temperatures below -20° F, corresponding to high altitude and low flight Mach number, were not obtained. At the higher altitudes, the minimum engine speed was sometimes limited by combustion blowout and the maximum engine speed by a turbine-outlet temperature of 1400° F at the hottest thermocouple.

CONTRACTOR

Thrust was measured with the tunnel balance scales and was also calculated from pressure and temperature measurements obtained at the exhaust-nozzle outlet. Air flow was calculated from pressure and temperature measurements made in the engine-inlet duct and at the exhaust-nozzle outlet. Both values of jet thrust and air flow are presented in the tabulated data; performance parameters presented in the tabulated data and the performance curves that involve thrust and air flow are calculated by using thrust measured by the balance scales and air flow measured at the engine inlet. The methods of calculation used in this report are the same as presented in reference 2.

#### RESULTS AND DISCUSSION

A summary of performance data, average pressures and temperatures throughout the engine, and lubrication and fuel-system data is presented in tables I, II, and III, respectively, for all altitudes, flight Mach numbers, and engine speeds at which data were obtained with the modified engine and a 170.6-square-inch exhaust nozzle. A comparison of average temperature patterns at the turbine outlet for both the original and modified engines showing the relation to the manufacturer's desired temperature distribution is presented in figure 4 for an altitude of 5000 feet, engine speed of 12,500 rpm, and a flight Mach number of 0.25. In order to conserve turbine life, operation of the original engine was limited to a maximum turbine-outlet temperature limit of 1250° F (1710° R). As a result of the modifications made to the engine, the temperature distribution at the turbine inlet was improved and the temperature limit raised to 1400° F (1860° R) as indicated by the hottest thermocouple. The average temperature pattern at the turbine outlet for the modified engine with a 1400° F limit (fig. 4) conformed more closely to the manufacturer's desired temperature distribution than did the original configuration. The data indicate that the temperature limit for the original engine was somewhat more conservative than that of the modified engine.

### Engine Performance

Effect of altitude. - The effect of altitude on engine performance is shown in figure 5 for data obtained at a constant flight Mach number of 0.25 and altitudes from 5000 to 45,000 feet. The trends of the performance curves for the modified engine followed closely those of the original engine. Jet thrust, net thrust, air flow, and fuel consumption are presented in figures 5(a), 5(b), 5(c), and 5(d), respectively.

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The specific fuel consumption based on net thrust (fig. 5(e)) was not appreciably affected at any engine speed when the altitude was raised from 5000 to 15,000 feet and was unaffected at engine speeds above 10,000 rpm when the altitude was raised to 25,000 feet; however, further increase in altitude above 25,000 feet raised the specific fuel consumption at all engine speeds.

The fuel-air ratio (fig. 5(f)) increased as the altitude was raised; the increase in fuel-air ratio became more pronounced at the high altitudes. The minimum fuel-air ratio occurred at an engine speed between 9000 and 10,000 rpm for each altitude.

The exhaust-nozzle-outlet total temperature (fig. 5(g)) increased at the high engine speeds as the altitude was raised. For engine speeds below approximately 11,000 rpm, an increase in altitude to 25,000 feet decreased the exhaust-nozzle-outlet temperature; however, for altitudes above 25,000 feet, the temperature increased considerably.

Effect of flight Mach number. - The effect of flight Mach number on engine performance is shown in figure 6 for data obtained at an altitude of 25,000 feet and flight Mach numbers from 0.25 to 1.07. For all engine speeds, raising the flight Mach number increased the jet thrust (fig. 6(a)), air flow (fig. 6(c)), and specific fuel consumption based on net thrust (fig. 6(e)).

Raising the flight Mach number from 0.25 to 0.53 decreased net thrust (fig. 6(b)) throughout the entire range of engine speeds presented. As flight Mach number was increased beyond 0.53, net thrust decreased at low engine speeds and increased at high engine speeds.

As the flight Mach number was raised, the fuel consumption (fig. 6(d)) increased at engine speeds above 10,000 rpm and decreased at lower engine speeds. The fuel-air ratio (fig. 6(f)) decreased at all engine speeds as the flight Mach number was raised from 0.25 to 0.86 but increased at high engine speeds with a further increase in flight Mach number.

Throughout the range of engine speeds, the exhaust-nozzle-outlet temperature (fig. 6(g)) decreased for flight Mach numbers up to and including 0.86 but increased slightly at high engine speeds with a further increase in flight Mach number.



#### Generalized Performance

The altitude performance data that were presented in figures 5 and 6 have been generalized to standard sea-level conditions by use of the factors  $\delta$ , ratio of absolute ambient static pressure to absolute static pressure corresponding to NACA standard atmosphere at sea level, and  $\theta$ , ratio of absolute ambient static temperature to absolute static temperature corresponding to NACA standard atmosphere at sea level. The generalized performance data are presented in figures 7 and 8. The concept of flow similarity and the application of dimensional analysis to the performance of turbojet engines has led to the development of these factors with which data obtained at several altitudes may be generalized. In the development of this method of generalization, the efficiencies of the engine components were considered to be unaffected by changes in altitude.

Effect of altitude. - The effect of altitude on generalized engine performance is shown in figure 7 for data obtained at a constant flight Mach number of 0.25 and altitudes from 5000 to 45.000 feet.

Jet thrust, net thrust, and air flow were the only performance data that generalized to a single curve at any engine speed or altitude for which data were obtained. Application of the generalization factors corrected the jet thrust (fig. 7(a)) and net thrust (fig. 7(b)) to a single curve at altitudes up to 15,000 feet for all engine speeds. At corrected engine speeds below 10,500 rpm, the jet thrust and net thrust generalized to a single curve at altitudes up to 25,000 feet. For all engine speeds, the corrected jet thrust and corrected net thrust increased as the altitude was raised above 25,000 feet. The air flow (fig. 7(c)) generalized to a single curve at altitudes up to 25,000 feet for all engine speeds; increase in altitude above 25,000 feet decreased the corrected air flow at all engine speeds.

Corrected fuel consumption (fig. 7(d)), corrected specific fuel consumption based on net thrust (fig. 7(e)), corrected fuelair ratio (fig. 7(f)), and corrected exhaust-nozzle-outlet total temperature (fig. 7(g)) increased markedly as the altitude was raised.

Failure of the thrust and air-flow data to generalize for all altitudes and corrected engine speeds is attributed to the change in compressor efficiency with altitude. Failure of variables depending upon fuel consumption (figs. 7(d) to 7(g)) to generalize



to a single curve for any engine speed or altitude at which data were obtained is attributed to changes in compressor and combustion efficiency with altitude.

Effect of flight Mach number. - The effect of flight Mach number on engine performance generalized to standard sea-level conditions is shown in figure 8 for data obtained at an altitude of 25,000 feet and at flight Mach numbers from 0.25 to 1.07. The effect of flight Mach number on the generalized performance was similar to the effect on the engine performance data presented in figure 5. The data presented in figure 8 do not represent the absolute generalized sea-level performance of the engine inasmuch as the application of the generalization factors did not correct the performance data for various altitudes to a single curve.

Comparison of original and modified engine performance. - Data showing the percentage change in the corrected values of net thrust and specific fuel consumption based on net thrust for the modified engine as compared to the original engine for several specific operating conditions are presented in the following table:

(a) Corrected engine speed, 13,000 rpm<sup>a</sup>; altitude, 25,000 feet.

Flight Mach number	Correcthrust (11 Original engine	Modi- fied	Change in corrected net thrust (percent)		umption net thrust,	Change in corrected specific fuel con- sumption based on net thrust (percent)
0.25 .53	2925 2760	<b>315</b> 0	.8 10	1.250 1.370	1.225	-2
.53 .73	2760	3040	10	1.400	1.355 1.400	- <u>1</u> .
.86	2925	3210	10	1.445	1.445	Ö
1.07	3050	<b>34</b> 90 ·	. 14	1.510	1.560	3

<sup>&</sup>lt;sup>a</sup>Engine speeds are the maximum speeds at which data were obtained over the complete range of test conditions.

(b	)	Corrected	engine	speed,	12,000	rpma; flig	ht Mach	number,	0.25.
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Altitude (ft)	Corrections (1) Crig- inal engine	_	corrected net thrust		mption	Change in corrected specific fuel con- sumption based on net thrust (percent)
5,000	2200	2320	5	1.175	1.165	-1
15,000	2200	2320	5	1.220	1.200	-2
25,000	2200	2400	9	1.280	1.230	-4
35,000	2340	2480	6	1.365	1.365	0
45,000	2525	2810	<b>11</b>	1.540	1.490	-3

Engine speeds are the maximum speeds at which data were obtained over the complete range of test conditions.

#### SUMMARY OF RESULTS

The following results were obtained from the altitude-windtunnel investigation of the modified X24C-4B turbojet engine at simulated altitudes from 5000 to 45,000 feet, simulated flight Mach numbers from 0.25 to 1.07, and engine speeds from 4000 to 12,500 rpm:

- 1. The average temperature pattern at the turbine outlet for the modified engine conformed more closely to the manufacturer's desired temperature distribution than did the original configuration.
- 2. A comparison of original and modified engine performance data showed that with the modified configuration a thrust increase of from 5 to 14 percent based on original engine output was obtained for several specific operating conditions.
- 3. Application of the generalization factors showed that performance variables depending upon fuel consumption that are obtained at one altitude cannot be used in predicting the values of these variables at any other altitude; however, thrust and air-flow values can be predicted for a limited range of altitudes from data taken at one altitude.

4. The specific fuel consumption based on net thrust increased at all engine speeds at a flight Mach number of 0.25 when the altitude was raised above 25,000 feet. Increasing the flight Mach number raised the specific fuel consumption based on net thrust at all engine speeds.

Flight Propulsion Research Laboratory,
National Advisory Committee for Aeronautics,
Cleveland, Ohio, December 22, 1947.

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Approved:

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jgm

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78	Corrected exhaust-norsine of the correction of $_{ m GO}$	1262	1245	1220	1205	1241	1428	1497	1590	1140	1179	1175	1195	1202	1350	1427	1510	1149	1170	1194	1210	1187	1267	1417
23	oltar rla-feul betoerro0 0\(a\lambda)	9210.0	0110	.0109	.0103	.0104	1210	.0142	9010	9010	.0104	2600.	00003	7600°	0114	°C124	. CL 38	30.00	0125	0125	0110°	0110	9010	00123
22	Corrected specific fuel consumption of the consumption of the consumption of the consumption (in thrust))	7.577	3.512	2.621	1.548	1.272	1.144	1,141	1.170	7.391	4 .406	2,087	1.582	292°T	1,207	1,170	1.170	16191	253.0	4.665	2,345	2,271	1,345	1,196
12	Corrected fuel consumption $M_{\Gamma} \setminus (0.10)$	591	871	1004	1148	1683	2629	2967	5437	643	793	1083	1300	1655	2218	2564	2960	3600	831	989	1306	1290	1863	2477
20	Corrected cowl-inlet air flow, (W <sub>B,l</sub> 40)/5 (lb/sec)	12	30	3	37.51	45.5	33	3	9 5	19	2 2	32	38	47	2 (3	57	S;	3.5	18	2	33	22.5	5.4	3
18	Corrected net thrust $\mathbb{F}_{\mathbf{n}} \setminus \mathbb{S}$	78	248	383	615	1323	2299	2600	2937	84	180	519	822	1831	1837	2191	2529	2082	87	212	557	999	1385	2021
18	Corrected let thrust [4] (1)	129	337	499	1092	1561	2641	2955	3322	523	357	776	1157	1711	2323	2709	3088	7545	244	389	840	936	1815	2576
17	Corrected engine speed W/VE (rpm)				9,128												12,288	12,775	2000	6,312	8,470	434.0	10,520	11,583
16	Exhaust-nozzle-outlet total temperature (Ro)	1218	1204	1184	1168	1207	1381	1448	1523	1115	1146	1141	1139	1173	1286	1358	1439	1522	1000	1079	1079	1072	1144	1273
15	Fuel-sir ratio, f/a	0.0124	.0113	.0106	010	1010	0127	.0137	.0152	20 20 20 20 20 20	1010	000	68C0°	20092	36	3110.	.0132	.0147	0110	0113	9000°	6000	9600°	.011
14	Specific fuel consumption based on net thrust, $^{\mathrm{M}}\Gamma^{\mathrm{F}_{n}}$ (lb/(hr)(lb thrust))	7.400	3,459	2,584	1,837	1.255	1,120	1,122	1,145	7,292	4 ,349	2.056	1,545	1,250	19767	1,142	1,143	1,166	0000	4 ,433	2,214	2,159	1,279	1,136
13	Fuel consumption, Wr (lb/hr)	481	200	819	935	1374	2142	2415	2786	525	648	884	1060	1348	1800	2081	2405	2766	444	532	693	693	966	1323
72	Exhaust-nozzle-outlet air flow, Wa,8 (lb/sec)	10.57	16.92	20.87	31.42	37.58	46.31	48.46	50.43	14.61	18.20	26.51	33,97	40,56	46.05	48.71	51,04	52.64	0.83	13.28	19.76	19.66	29,62	33,16
11	Cowl-inlet air flow Wa,l (lb/sec)	ន្ទ្រ	74	ซ	38.09	37	44	48	85	77	45	26	33	6;	4 4 6 6	48	င္သ	ŝ	° C	123	13			
10	Net thrust, F <sub>n</sub> , (lb)				509																			
6	fall thrust, Fj (16)				625 904																			
8	delculated jet thrust (1b)	113	287	426	627	1331	2201	2487	2794	16	305	640	1006	1449	2044	2312	2639	2979	748	224	201	484	1064	1497
6	Compressor-inlet indicated temperature (R <sup>O</sup> )	202	2 2	506	S 50 40 40 40 40 40 40 40 40 40 40 40 40 40	203	20°5	505	500	514	5	510	501	200 200 300	404 104	i S	205	200	474	474	460	473	475	474
9	Engine apeed, N	4,000	900	7,000	000	10,000	11,000	12,000	12,440	200	9		ີດ	ō,	200	'n	o.	ດ ີ ຈ	200	000	8,000	000 a	ŝ	11,000
2	Tunnel temperature, To				474								474	474	47.7	484	489	496					453	465
4	Tunnel static pressure po (lb/sq ft abs.)				1752																			
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TABLE I - PERFORMANCE DATA FUR MODIFIED X24C-4B TURBOJET ENGINE WITH 170.6-SQUARE-INCH EXHAUST NOÇZLE

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54	Corrected exhaust-nozzle- outlet total temperature $(R)$	686 8858 8858 8858 11085 11085 11086 11086 11088 11088 11088 11088 11088 11088 11088 11088 11088 11088 11088 11088 11088
23	Corrected fuel-air ratio (s/1)	0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098 0.0098
22	Corrected specific fuel thrust, W <sub>1</sub> (F <sub>N</sub> Ve) (Lb) (hr thrust))	13. (a) (b) (b) (c) (c) (c) (c) (d) (d) (d) (d) (d) (d) (d) (d) (d) (d
21	Corrected fuel consumption	111862 111862 11862 11879 11879 11879 11879 11879 11879 1189 118
20	Corrected coml-inlet air flow, (Wa,146)/5 (lb/sec)	26.b6 45.86 45.86 45.86 45.86 45.86 45.86 45.86 45.86 45.86 45.86 45.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86 46.86
19	Corrected net thrust $\mathbb{F}_{n}/\delta$ (1b)	1.351 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056 1.056
18	Corrected let thrust Pylo (1b)	8 31 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8
17	Corrected engine speed N/46 (rpm)	9 0 0 7 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
16	Exhaust-nozzle-outlet total temperature, 7g ( <sup>o</sup> R)	568 648 854 854 854 852 630 630 630 630 630 630 630 630 630 630
15	Fuel-air ratio, f/a	0.0080 0.0070 0.0070 0.0070 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.
74	Specific fuel consumption of AT/Yn (15 thrust, Wr/Yn (15 thrust))	(a) 10,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11,5000 11
13	Fuel consumption, Wr (lb/hr)	8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9
12	Exhaust-nozzle-outlet air flow, Wa,8 (lb/sec)	11.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1
12	woll the fall flow (15 /dl) [,gW	10.86 112.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86 10.86
10	Net thrust, Pn (lb)	1129 120 120 120 120 120 120 120 120
6	Scale jet thrust, F; (1b)	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
8	Selculated jet thrust	119 200 305 472 710 1104 1104 1179 220 220 220 220 220 220 220 220 220 22
2	telni-aceseardmoo findicated temperature (AO) (AC)	44444444444444444444444444444444444444
9	Engine apeed, N (rgm)	5,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,000 111,0
5	Tunnel temperature, To (9R)	4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6
4	Tunnel static pressure po (lb/sq ft abs.)	100000000000000000000000000000000000000
3		2
2	Ram-pressure ratio, PS/PO	0851141881148881888888888888888888888888
1	epnatate (4J)	88888888888888888888888888888888888888
_	, uny	0-000-000-00-000-000-000-00-00-00-00-00
	-	

TABLE I - PERFORMANCE DATA FOR HODIFIED X24C-4B TURBOJET ENGINE WITH 170-SQUARE-INCH EXHAUST NOZZLE - Concluded

CALL



apata not obtained.

TABLE II - AVERAGE PRESSURES AND TEMPERATURES THROUGHOUT MODIFIED (Stations identified

Compressor stator-atage   Static pressure, P3   Compressor stator-atage   St		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	-19	20
1	<u> </u>	1	~		8	۱ř				-	10	9	12	10	7.4	13	10	1./	18	.19	20
1 5,000 1,000 0,00 1753 465 4,000 156 493 1759 1756 560 1768 1768 1768 1769 1765 1869 1879 1869 1879 1869 1879 1879 1879 1879 1879 1879 1879 187	ur	ltitude (ft)	pressure ratio	Mach numb	static press (sq ft abs.)	ol temper	o speed, N, r	thrust, Fn	ated tempera (OR)	pressure,   ft abs.)	prossure, ft abs.)	cated temperat	l pressure, sq ft abs.)	nressure, 1 ft abs.)a	c pressure, q ft abs.)		stat:	ic pr	essur	ө, р <sub>З</sub>	5e
2 5,000 1.011.10 1762 469 5,000 1264 499 1769 1756 504 1769 1769 1789 1787 1829 1879 1814 1849 1891 5 5,000 1.011.10 1762 469 6,000 205 489 1771 1749 504 1771 1771 1755 1774 1737 1829 1849 1849 1849 1849 1849 1849 1849 184	Ĕ	4	5 4	Ξ×	5 5	ĘĘ	ជ	ž	II T	ž.	St C	45	T.	£C.	St (J	1	2	3	4	5	6
54   15,000   1.419   .73   1190   503   12,000   1564   521   1697   1514   521   1689   1672   1558   1458   1598   1859   2147   2521   2873	1233456678901123456678901123456678901123456789011234567890112322222222222356789041243445678490152	5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 5,000 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1.053 1.053 1.053 1.053 1.053 1.053 1.053 1.053 1.053	09 100 111 113 166 188 244 244 245 266 267 274 244 245 255 266 267 277 273 273 273 273 273 273 27	1753 1752 1752 1752 1752 1752 1752 1752 1753 1753 1753 1753 1757 1760 1760 1760 1760 1190 1190 1190 1190 1190 1190 1190 11	466 469 469 474 477 484 477 486 486 486 487 474 474 474 474 474 489 496 454 453 453 453 463 463 463 463 464 465 463 472 472 474 474 474 474 474 474 474 475 476 477 477 478 479 479 479 479 479 479 479 479 479 479	4,000 5,000 7,000 8,000 9,000 11,000 11,500 12,440 4,000 5,000 6,000 7,000 11,000 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500 11,500	65 126 205 317 751 1095 2152 2152 2157 430 257 430 257 430 257 430 257 430 257 430 2152 2373 18 420 313 3213 779 1165 1378 1795 11673 11673 1178 11673 1178 1178 1178 1178 1178 1178 1178 11	498 499 502 502 503 503 503 503 503 503 503 503 503 503	1767 1769 1771 1773 1775 1778 1778 1820 1821 1820 1825 1825 1827 1847 1853 1853 1853 1242 1243 1246 1243 1246 1253 1246 1253 1246 1253 1246 1253 1246 1253 1246 1253 1246 1253 1246 1253 1246 1253 1246 1253 1246 1253 1246 1253 1246 1253 1246 1253 1246 1253 1256 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1257 1248 1248 1257 1248 1248 1257 1248 1248 1257 1248 1248 1257 1248 1248 1257 1248 1248 1248 1257 1248 1248 1248 1248 1248 1248 1248 1248	1758 1756 1749 1724 1702 1616 1619 1619 1619 1619 1619 1619 161	502 504 504 504 505 506 505 507 505 505 505 500 514 511 501 501 501 501 501 502 474 474 474 474 474 474 474 47	1768 1773 1773 1773 1773 1773 1776 1791 1823 1823 1823 1823 1823 1823 1823 182	1768 1779 1771 1778 1779 1795 1820 1821 1825 1845 1845 1845 1845 1847 1848 1238 1237 1242 1239 1247 1246 1251 1255 1258 1427 1431 1429 1432 1426 1427 1431 1429 1432 1426 1427 1431 1429 1432 1427 1431 1431 1429 1432 1427 1431 1431 1431 1431 1431 1431 1431 143	1762 1759 1755 1759 1750 1695 1695 1695 1697 1807 1807 1797 1797 1797 1797 1797 1797 1797 17	1781 1787 1794 1787 1808 1676 1598 1823 1832 1836 1843 1823 1837 1725 1612 1246 1253 1245 1246 1253 1245 1246 1253 1245 1246 1253 1245 1246 1253 1245 1246 1253 1245 1253 1245 1246 1253 1245 1253 1245 1253 1245 1253 1245 1253 1245 1253 1245 1253 1245 1253 1245 1253 1253 1253 1253 1253 1253 1253 125	1809 1829 1865 1921 1963 1953 1953 1953 1953 1955 1955 1955 195	1837 1879 1935 2048 2011: 2146 2105 2035 1942 11922 2041 1222 2041 1222 2189 2232 2175 2056 1439 11366 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256 11256	1866 1914 1984 2035 2350 2350 2350 2257 22175 1914 2330 2450 2230 2450 2233 1303 1344 1521 1521 1521 1521 1521 1521 1521 15	1887 1949 2041 2139 2266 2428 2603 2717 2657 2612 1935 2196 2330 2541 2717 2805 2767 2762 2768 2767 2769 1324 1374 1619 1753 1838 1838 1841 1753 1852 1993 1753 1852 1993 1852 1993 1852 1993 1852 1993 1852 1993 1852 1993 1852 1993 1993 1993 1993 1993 1993 1993 199	1908 1991 2104 22317 2618 2878 3034 3077 3013 1970 2042 2168 2294 2464 2999 3147 3133 3154 3153 1414 1150 1717 1726 2123 2165 22125 2446 2411 11871 2165 22125 2446 2411 11971 2165 22125 2446 2411 2191 2191 2191 2191 2191 2191 2191

\*Kanufacturer's instrumentation.

bData not obtained for turbine stator-stage static pressures.

CData not obtained.



224C-48 TURBOJET ENGINE WITH 170.6-SQUARE-INCH EXHAUST NOZZLE in figure 5.}

21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	
	resso atic (lb/s	press		рз	temperature	temperature	abs.)	ssure, P4	aba.)	sure, P5	sure, P5	temporature	temperature	sure, P7	suro, P7	abs.)	tomperature	sure, Pg abs.)	ssure, Pg abs.)	
7	8	9	10	11	Indicated T <sub>1,4</sub> (OR)	Indicated T1.4 (OR)*	Total pres (1b/sq ft	Pr	Static pro	pres ft	Total pres (1b/sq ft	Indicated T <sub>1,7</sub> (OR)	Indicated T <sub>1,7</sub> (OR)a	Total pressi (1b/sq ft al	Total pres (1b/sq ft	Static pre (1b/sq ft	Indicated Ti,8 (OR)	Total pros (1b/sq ft	Static pre (1b/sq ft	Run
1943 2041 2181 2336 2555 2822 3146 3386	1978 2104 2273 2470 2731 3061 3463 3816	1999 2139 2336 2562 2871 3273 3772 4252	2013 2174 2386 2063 3019 3512 4132 4801	1985 2132 2336 2597 2984 3505 4209 5027	532 550 573 598 626 658 693	534 553 576 603 632 666 702 737	2050 2229 2483 2800 3257 3863 4673 5616	2049 2231 2484 2808 3259 3871 4667	2032 2201 2440 2743 3174 3762 4528 5451	2010 2167 2392 2674 3076 3632 4371 5263	2006 2167 2392 2678 3083 3643 4378	1234 1227 1211 1209 1199 1205 1234	1306 1301 1285 1279 1279 1290 1311	1809 1841 1891 1953 2050 2202 2429	2414	1786 1799 1822 1863 1919 2007 2158	1216 1217 1200 1180 1162 1180 1196	1801 1834 1881 1946 2043 2193 2408	1756 1761 1768 1777 1793 1812 1866	1 2 3 4 5 6 7
3464 3463 3464 1991 2091 2246 2407	3942 3998 4069 2027 2147 2330 2526		5125 5373 5681 2041 2190 2422 2695	5414 5786 6280 1984 2119 2337 2597	731 746 765 780 540 556 578 602	757 776 790 542 560 580	6108 6494 6931 2055 2231 2509 2829	5618 6118 6504 6927 2055 2232 2506 2829	5936 6313 6727 2033 2196 2455 2761	5735 6110 6551 2009 2154 2405 2688	5273 5745 6128 6565 2005 2161 2408 2688	1332 1399 1485 1578 1095 1129 1157	1421 1504 1610 1696 1147 1193 1226 1220	2764 2970 3152 3363 1807 1836 1893 1960	2739 2950 3118 3309 1801 1830 1887 1949	2392 2546 2686 2851 1780 1788 1835 1863	1300 1363 1428 1501 1078 1113 1143 1149	2731 2916 3092 3293 1804 1828 1884 1955	1962 2038 2112 2229 1758 1749 1759 1784	9 10 11 12 13 14 15
2619 2964 3288 3506 3485 3527 3576	2788 3196 3619 3949 3921 4020 4132	2929 3407 3935 4414 4379 4555 4752	3062 3647 4308 4984 4921 5224 5555	2985 3604 4365 5231 5153 5505 5977	627 653 686 716 724 744 762	634 660 694 723 731 752 773	3273 3995 4878 5849 5762 6224 6712	3281 3999 4872 5850 5752 6237 6730	3192 3876 4723 5673 5581 6045 6523	3096 3745 4555 5475 5388 5836 6310	3102 3756 4566 5484 5393 5850 6326	1167 1153 1203 1289 1301 1373 1469	1237 1233 1270 1372 1381 1469 1576	2046 2238 2479 2827 2798 3009 3214	2042 2239 2471 2809 2781 2992 3189	1924 2035 2203 2455 2427 2553 2748	1135 1130 1160 1252 1268 1338 1416	2043 2236 2472 2800 2768 2962 3164	1778 1810 1855 1913 1906 1963 2036	16 17 18 19 20 21 22
3562 1366 1442 1249 1830 1831 2070 2239	4182 1387 1492 1619 1963 1964 2253 2485	4886 1401 1485 1662 1977 2077 2408 2725	5836 1401 1527 1690 2182 2183 2577 3006	6442 1359 1478 1633 2146 2147 2570 3091	783 502 515 540 590 594 625 662	794 502 516 543 594 600 633 669	7114 1413 1562 1751 2350 2351 2848 3415	7110 1415 1562 1760 2358 2359 2851 3429	6906 1401 1540 1725 2290 2292 2768 3329	6716 1384 1508 1683 2221 2225 2668 3218	6734 1384 1513 1683 2224 2229 2679 3222	1581 1050 1066 1088 1089 1098 1098	1689 1114 1138 1160 1159 1171 1173 1237	3414 1231 1261 1304 1426 1422 1540 1720	3372 1225 1259 1296 1414 1422 1542 1718	2903 1211 1226 1258 1318 1333 1406 1523		3349 1226 1252 1295 1423 1420 1539 1712	2118 1190 1192 1203 1221 1222 1228 1256	23 24 25 26 27 28 29 30
2387 2401 2408 2401 1563 1669 1767	2718 2774 2823 2894 1570 1690 1817	3056 3125 3302 3443	3492 3703 3929 4175 1514 1669 1831	3675 3971 4302 4569 1345 1479 1641	699 716 738 769 511 531 552	707 724 746 772 512 534 556	4140 4454 4763 5035 1438 1609 1810	4147 4457 4752 5047 1436 1612 1810	4024 4332 4620 4868 1409 1572 1760	3891 4189 4501 4768 1387 1535 1715	3897 4200 4513 4784 1387 1542 1715	1290	1373 1458 1562 1687 653 782 870	1990 2131 2278 2415 1233 1264 1307	1971 2119 2260 2394 1225 1260 1295	1718 1831 1943 2061 1218 1232 1251	1254 1323 1405 1512 654 741 829	1965 2100 2241 2375 1229 1256 1298	1324 1370 1427 1490 1187 1190 1199	31 32 33 34 35 36 37
1901 2084 2334 2524 2700 2756 2763	1978 2204 2510 2770 3038 3143 3192	2664 3009 3397 3558 3692	3840 4094 4333	4319 4692	671 710 738 763	584 617 642 679 718 746 773	2086 2474 3045 3682 4507 4880 5251	2084 2471 3052 3685 4502 4882 5255	2373 2925 3566 4368 4738 5101	1954 2302 2823 3429 4213 4579 4938	1957 2309 2837 3436 4220 4586 4949	884 930 970 1072 1235 1348 1465	936 988 1031 1143 1313 1446 1582	1363 1449 1597 1806 2140 2327 2508	1359 1443 1587 1798 2115 2305 2481	1279 1336 1427 1575 1832 1977 2136	867 921 955 1043 1197 1308 1400	1355 1436 1582 1786 2113 2286 2456	1209 1228 1247 1304 1445 1540 1648	38 39 40 41 42 43 44
2777 1943 2049 2285 2443 2682 2908 3126	3277 1950 2084 2288 2570 2858 3154 3485	3861 1943 2098 2330 2654 3020 3401 3865	2042 2309 2697 3133	5065 1443 1626 1887 2295 2795 3478 4414	788 531 575 597 614 648 686 728	795 533 578 601 619 656 691 735	5619 1654 1877 2198 2675 3271 4000 4960	5607 1655 1873 2183 2668 3267 3999 4956	5431 1589 1804 2098 2563 3128 3851 4799	5315 1549 1746 2018 2457 2999 3693 4618	5329 1549 1750 2025 2464 3006 3710 4630	1604 561 677 752 802 868 992 1210	1707 590 704 783 786 907 1044 1274	2701 1268 (c) 1380 1491 1656 1912 2337	2664 1253 (c) 1366 1486 1648 1902 2309	2291 1227 1260 1301 1359 1467 1646	1514 594 671 750 799 866 968 1162	2646 1252 (c) 1369 1480 1637 1891 2294	1759 1171 (c) 1206 1235 1261 1342 1543	45 46 47 48 49 50 51
3189 3246 3056 3260	3612 3724 3591	4076 4281 4217	4618 4907	4844 5231 5442	752 782 808	759 790 819 824	5461 5893 6092 6230	5456 5907 6097 6238	5291 5727 5918	5108 5531 5728 5865	5115 5545 5741 5883	1340 1454 1593	1412 1543 1710 1729	2578 2578 2811 (c) (c)	2562 2562 2781 (c) (c)	2190 2380 2352 2535	1295 1410 1511 1526	2540 2754 (c)	1690 1830 (c)	53 54 55 56



TABLE II - AVERAGE PRESSURES AND TEMPERATURES THROUGHOUT MODIFIED X240-4B (Stations identified

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20
Run	ltitudo ft)	Ram-pressure ratio $^{P_{2}/p_{0}}$	Flight Mach number Mo	Tunnel static pressure po (1b/sq ft abs.)	Tunnel temperature To (OR)	Engine apeed, N, rpm	et thrust, F <sub>n</sub> (1b)	Indicated temperature . Ti, 1 (9R)	Total pressure, Pl	Static pressure, Pl (1b/sq ft abs.)	Indicated temperature Ti,2 (OR)	Total pressure, P2 (1b/sq ft abs.)	Total prossure, P <sub>2</sub> (1b/sq ft abs.) <sup>a</sup>	Static pressure, P2 (1b/sq ft abs.)		(1b	c pre /sq f	tator ssure t abs	, P3 .)	
-	(r						Š.								1	2	3	4	5	5
5785596616226346656677127744786667772774478681888886677117227744786888886687711723774478688888668771172377447868888866877117237744786888886687711723774478688888888888888888888888888888888	25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000 25,000	1.042 1.041 1.041 1.042 1.046 1.049 1.051 1.051 1.207 1.202 1.209 1.210 1.210 1.220 1.220 1.210 1.211 1.210 1.220 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.420 1.630 1.620 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005 2.005	.24 .24 .24 .26 .25 .26 .27 .26 .53 .53 .53 .53 .53 .53 .72 .72 .72 .73 .73 .73 .73 .73 .74 .73 .74 .73 .74 .73 .74 .73 .74 .73 .74 .74 .75 .76 .76 .77 .77 .77 .77 .77 .77 .77 .77	778 7788 7788 7786 7786 7786 7787 7811 7781 778	483 4871 494 466 466 4475 466 4475 453 445 451 453 445 453 445 453 445 453 445 453 445 453 445 453 445 453 445 453 445 453 445 453 445 453 445 453 445 453 445 453 445 453 445 453 445 453 445 453 445 453 445 453 445 453 445 453 445 453 445 453 445 453 445 453 445 453 445 453 445 453 445 453 445 453 445 453 445 445	4,000 5,000 6,000 9,000 11,000 11,000 11,000 12,000 6,000 7,000 6,000 7,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 11,000 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11,000 11,	164 45 89 144 230 393 393 6879 1036 879 11257 -55 50 11257 778 954 41135 -1213 -151 437 424 816 81285 -244 248 479 944 4479	450 449 447 445 4443 4443 4444 445 445 445 465 465 465 467 472 472 472 472 472 472 472 472 472 47	812 812 815 816 817 819 819 820 825 824 938 949 949 948 952 1100 1108 1104 11104 11104 1121 1121 1121 1121 11	807 807 802 7993 767 771 754 735 723 921 929 924 929 921 875 843 845 845 1093 11064 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 11054 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1027 1036 1126 1133 1126 1133 1126 1133 1126 1133 1126 1133 1133	850 883 919 961 1003 1067 (c) (c) (c) 950 1024 1058 1134 1257 1125 1239 1136 1141 1252 1239 1145 1454 1334 1454 1516 1516 1527 1943 2083 2108	862 898 947 1010 1074 1165 1168 1046 1091 1330 1422 1436 1350 1436 1363 1457 1552 1458 1457 1552 1458 1457 1552 1458 1457 1552 1458 1457 1458 1457 1458 1458 1458 1458 1458 1458 1458 1458	82820448) 1084480 108477335077977976566770771441335676781145405077977976662402402405077977976662402402402402402402402402402402402402402

AVanufacturer's instrumentation.



bData not obtained for turbine stator-stage static pressures.

CData not obtained.

TURBOJET ENGINE WITH 170.5-SQUARE-INCH EXHAUST NOZZLE - Continued in figure 3.)

21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	
	tic:	oress	itor-: ure, abs.	рз`	cated temperature (OR)	cated temperature (OR)a	al pressure, P4 /aq ft abs.)	l pressure, P4 sq ft abs.)a	ic pressure, p4 sq ft abs.)	1 prescure, Ps	al pressure, P <sub>5</sub>	cated temporature (OR)	cated temperature (OR)a	prossure, P <sub>7</sub>	l pressure, Pr	c pressure, pr q ft abs.)	(OR)	pressure, Pg q ft abs.)	ic pressure, pg sq ft abs.)	
7	6	9	10	11	Inds T1,4	Ind!		Total (1b/se	Stat (1b/	Total (15/5	Totu (1b/	Indl T1,7	Ind! Tj,7	Total (1b/s	Tota (1b/	Stati (1b/s	Tr. T	rotal (1b/s	Stat (1h/	Run
898	919 919 962 1313 1313 1313 (c) (c) (c) (c) (c) 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 1313 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1069 1073 1304 1409 1641 633 725 819 843 843 849 1074 959 1074 959 1075 1245 548 648 853 895 1245 1354 1475 1354 1475 1245 1245 1245 1245 1245 1245 1245 124	1200 1153 1161 1130 1136 1137 11478 11478 11478 1686 658 890 951 1020 1141 11438 1546 6169 853 951 1052 1147 11438 1546 660 1052 1291 1153 1153 1153 1153 1153 1153 1153 11	808 827 854 889 96 1051 1188 1198 615 837 912 1475 1083 1242 1475 1858 871 1097 1136 1136 1136 1136 1136 1136 1136 113	806 851 851 1402 1186 1375 1402 1046 1375 1402 1186 1375 1402 1186 1375 1402 1186 1372 1606 11372 1608 11372 1608 1908 1908 1908 1908 1908 1908 1908 19	794 804 818 846 847 952 (c) (c) 1420 792 851 1420 813 828 851 1591 11591 11591 11591 11591 11591 11591 11591 11691 11701 11800 11800 11800 11800 11800 11800 11800 11800 11800 11800 11800 11800 11800 11800 11800 11800 11800 11800 11800 11800 11800 11800 11800 11800 11800 11800 11800 11800 11800 11800 11800 11800 11800 11800 11800 11800 11800 11800 11800 11800 11800 11800 11800 11800 11800 11800 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1059 1057 784 777 797 797 1059 1057 1109 797 1308 784 797 797 797 797 797 1308 784 797 797 797 797 797 797 797 797 797 79	57 58 59 61 62 64 65 66 67 68 97 71 2 73 74 5 67 77 8 8 2 8 3 4 8 6 6 8 7 9 9 1
1865 15 2048 21 2217 24 2407 25 2428 25 2456 25 2316 24 2527 26 2745 25 2949 32 3048 34 3006 35	957 189 421 703 773 865 928 407 682 970 287	2020 2309 2625 3027 3153 3315 2478 2816 3196 3646 3886 3886	2055 2414 2851 3428 3646 3914 4167 2471 2893 3407 4062 4414 4604	1682 2119 2773 3590 3865 4252 4561 1802 2393 3175 4188 4639 4935	592 628 659 704 726 748 774 603 640 681 726 749	597 634 668 711 734 758 780 608 647 669 733 757 781	1990 2505 3171 4021 4356 4727 5059 2241 2878 3707 4695 5232	1992 2499 3132 4019 4364 4737 5040 2236 2872 3710 4702 5230 5561	1899 2390 2299 3896 4233 4604 4896 2116 2735 3554 4548 5072 5388	1913 2288 2928 3752 4087 4456 4784 2013 2608 3404 4375 4892 5209	1823 2295 2942 3759 4094 4470 4901 2020 2618 3421 4389 4903 5223	704 798 959 1198 1316 1440 1578 587 731 929 1207 1342 1452	743 839 1014 1267 1399 1542 1657 593 757 970 1271 1420 1536	1037 1205 1455 1846 2034 2237 2402 1104 1323 1698 2193 2474 2642	1027 1196 1457 1851 2027 2224 2386 1316 1682 2175 2442 2618	934 1044 1253 1589 1736 1907 2048 971 1138 1445 1870 2105 2240	700 792 927 1145 1274 1374 1497 592 723 909 1160 1300	1025 1191 1447 1837 2007 2198 2367 1092 1308 1673 2164 2433 2693	820 863 925 1130 1235 1358 1467 836 897 1103 1438	92 93 95 95 97 98 99 100 102 103 104

NACA\_\_

TABLE II - AVERAGE PRESSURES AND TEMPERATURES THROUGHOUT MODIFIED X240-4B (Stations identified

	\ 1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20
п	Altitudo (ft)	Ham-pressure ratio $ ho_2/ ho_0$	Flight Mach number Mo	Tunnel static pressure po (1b/sq ft abs.)	Tunnol temperature To ( <sup>O</sup> R)	Engine speed, N, rpm	t thrust, Fn (1b)	Indicated temperature T1,1 (OR)	Total prossure, Pl	tatic pressure, pl	Indicated temperature Ti,2 (OR)	rotal pressure, P <sub>2</sub> (1b/sq ft abs.)	lotal pressure, P2	Static pressure, po (1b/sq ft abs.)		tati	le pr	ressi ft a	cor-st ire, p	
Run							No		_	ຜ~		7	-	<u> </u>	1	2	3	4	5	6
106 107 109 110 1112 112 113 114 115 119 121 123 124 125 127 129 130 131 133 134 135 135 135 135 141 142 143 144 145 145 145 145 145 145 145 145 145	\$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 \$5,000 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 $<sup>^{\</sup>mathbf{a}}$ Manufacturer's instrumentation.



bData not obtained for turbine stator-stage static pressures.

<sup>&</sup>lt;sup>c</sup>Data not obtained.

TURBOJET ENGINE WITH 170.6-SQUARE-INCH EXHAUST NOZZLE - Concluded in figure 3.)

21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	
st	atic (lb/s	pres	ator-: sure, abs.	) <sup>P3</sup>	Indicated temperature	Indicated temperature T <sub>1,4</sub> (OR) <sup>a</sup>	Total pressure,. P4 (1b/sq ft abs.)	otal pressure, P4	Static pressure, p <sub>4</sub> (lb/sq ft abs.)	Total pressure, P <sub>5</sub> (1b/sq ft abs.) <sup>b</sup>	Total pressure, P5 (1b/sq ft abs.) <sup>a</sup>	Indicated temperature Ti,7 (OR)	ndicated temperature	otal prossure, P7	Total pressure, P7 (1b/sq ft abs.)	Static pressure, p7 (1b/sq ft abs.)	Indicated temperature	Total pressure, Pg (1b/sq ft abs.)	Static pressure, pg (1b/sq ft abs.)	Run
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TABLE III - LUBRICATION AND FUEL-SYSTEM DATA FOR MODIFIED X240-4B TURBOJET ENGINE WITH 170.6-SQUARE-INCH EXHAUST NOZZLE

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TABLE III - LUBRICATION AND FUED-SYSTEM DATA FOR MODIFIED X24C-4B TURBOJET ENGINE WITH 170.6-SQUARE-INCH EXHAUST NOZZIE -

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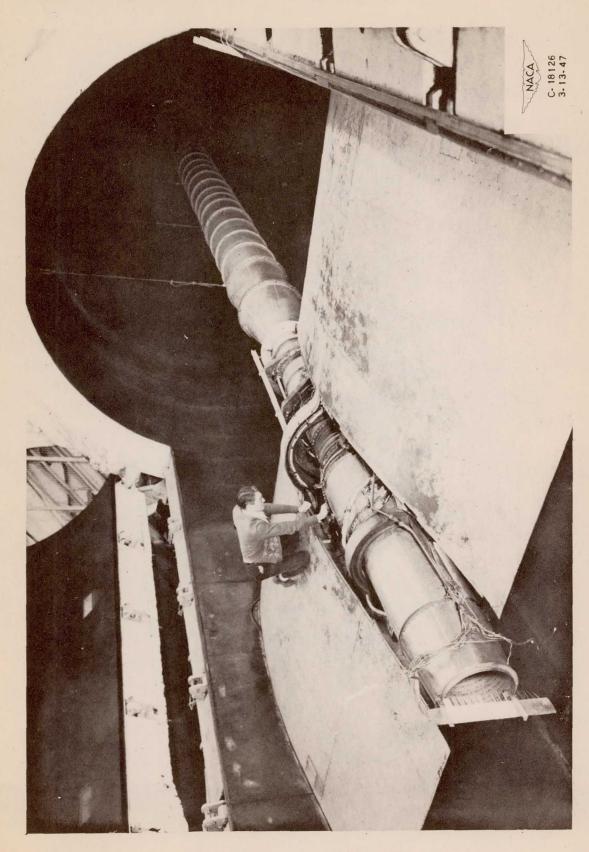
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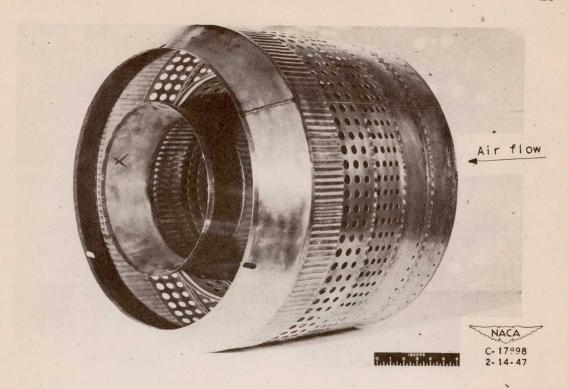
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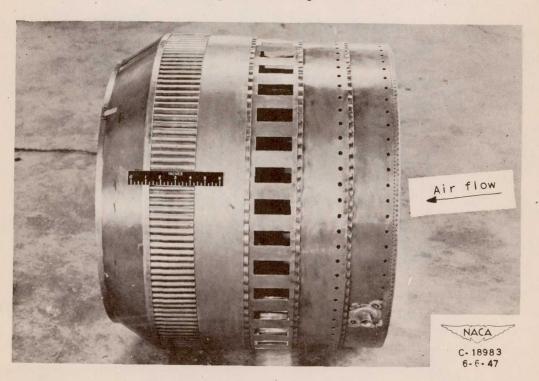
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altitude wind tunnel. - Installation of X24C-4B turbojet engine in Figure 1.



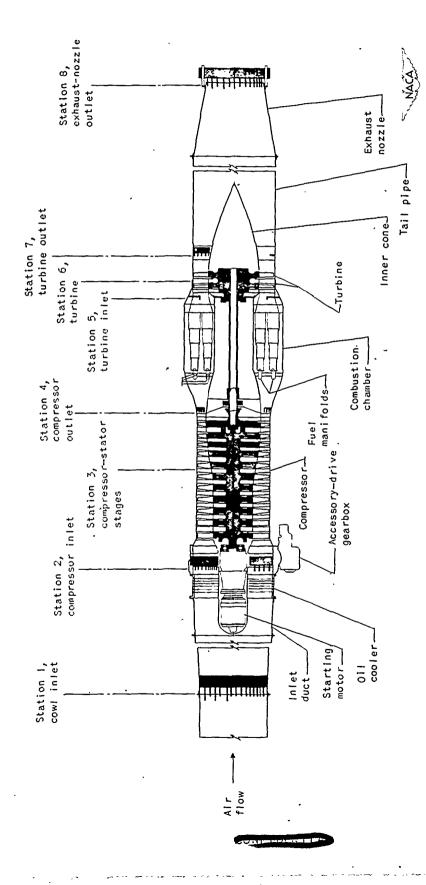
(a) Original configuration.



(b) Modified configuration.

Figure 2. - Comparison of original and modified combustion chambers.

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- Location of instrumentation installed in X24C-4B turbojet engine. Figure 3.

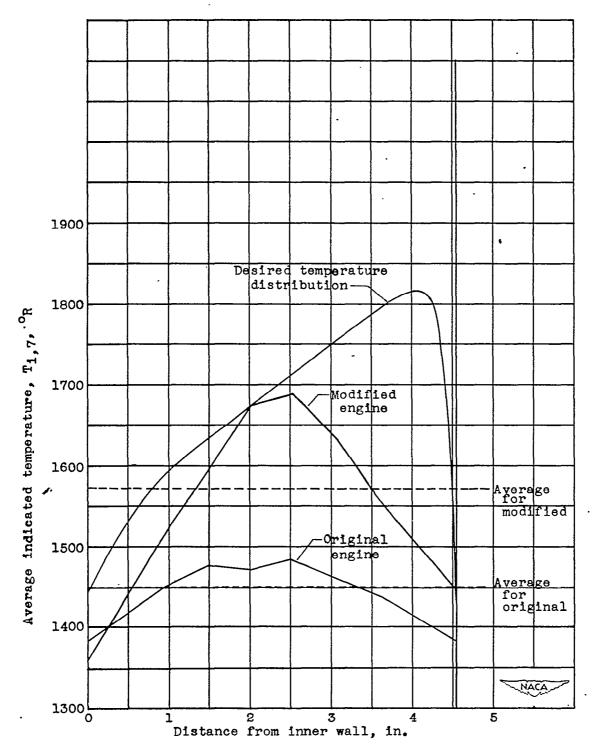


Figure 4. - Comparison of average temperature patterns at turbine outlet for original and modified engines and relation to manufacturer's desired temperature distribution as calculated from blade stress considerations. Altitude, 5000 feet; engine speed, 12,500 rpm; Mach number, 0.25.

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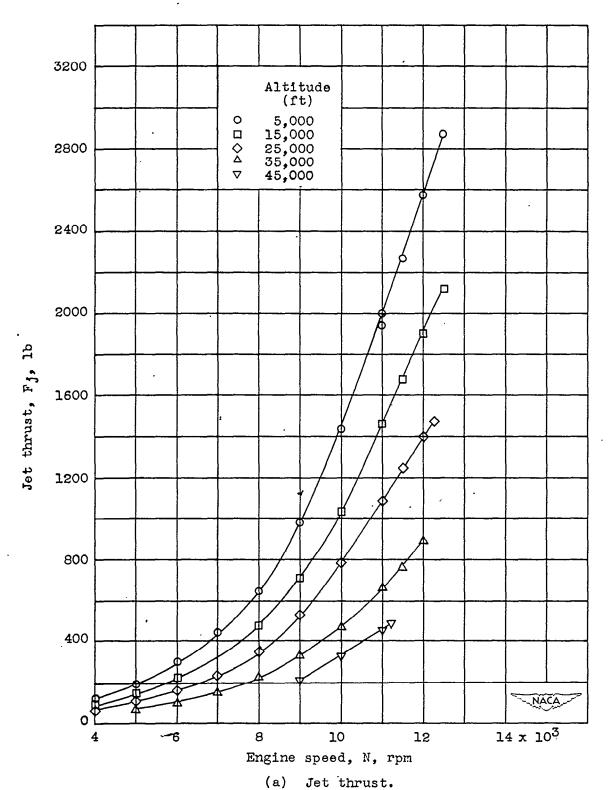


Figure 5. - Effect of altitude on variation of turbojet engine performance with engine speed. Flight Mach number, 0.25.

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Figure 5. - Continued. Effect of altitude on variation of turbojet engine performance with engine speed. Flight Mach number, 0.25.

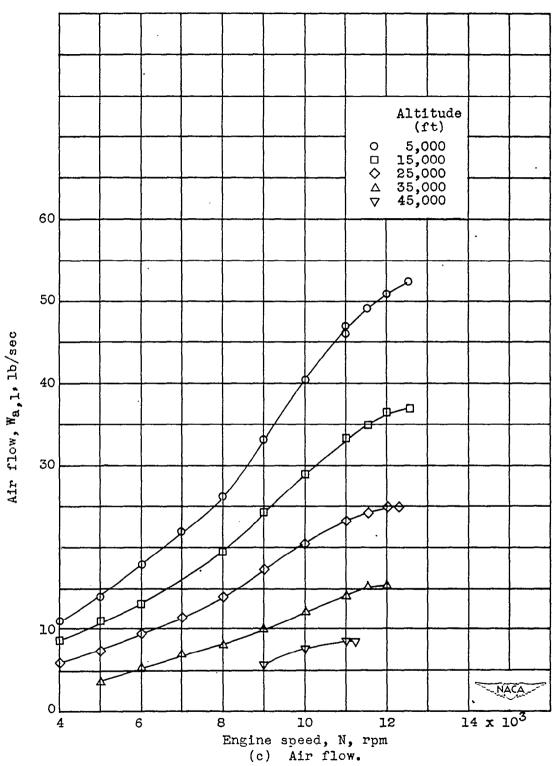


Figure 5. - Continued. Effect of altitude on variation of turbojet engine performance with engine speed. Flight Mach number, 0.25.

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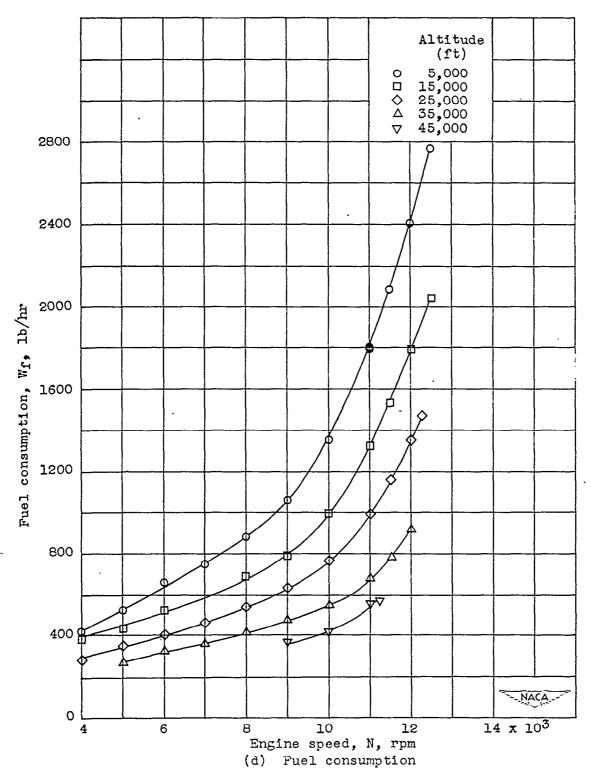
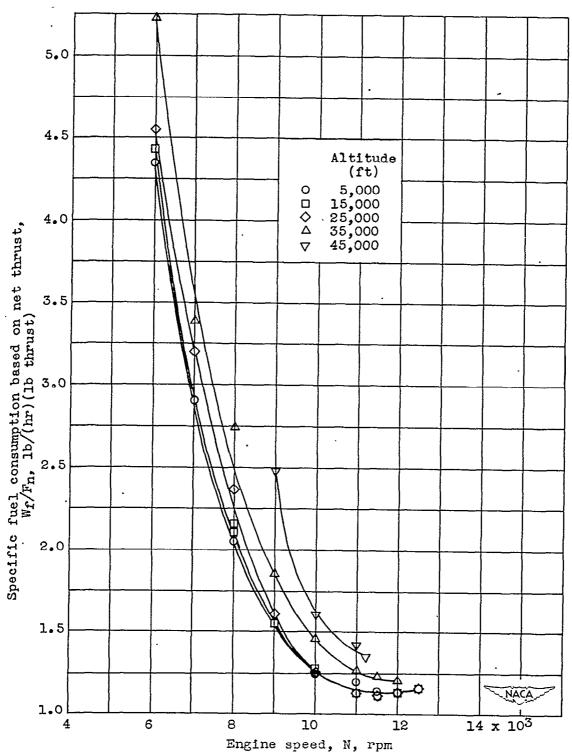


Figure 5. - Continued. Effect of altitude on variation of turbojet engine performance with engine speed. Flight Mach number, 0.25.

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(e) Specific fuel consumption based on net thrust.
Figure 5. - Continued. Effect of altitude on variation of turbojet engine performance with engine speed. Flight Mach number, 0.25.

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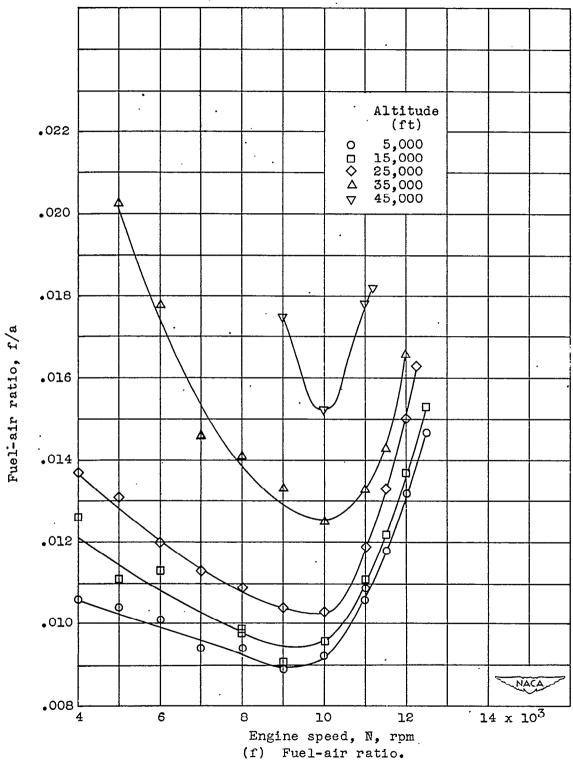
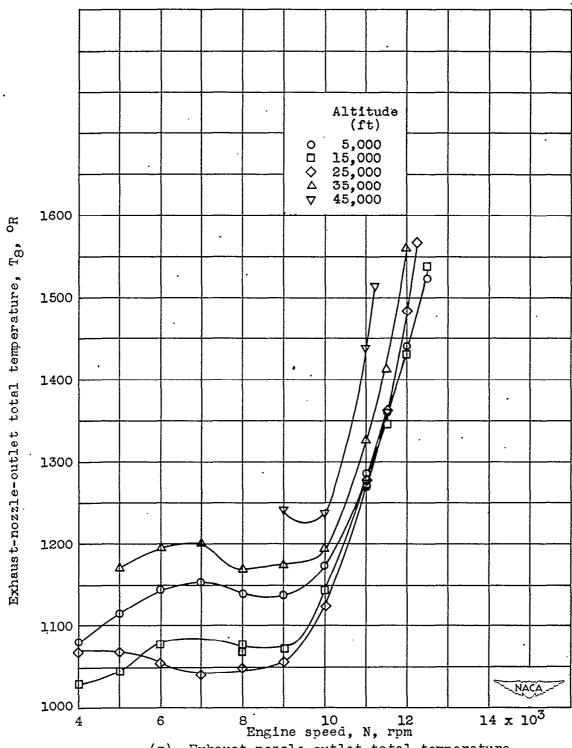


Figure 5. - Continued. Effect of altitude on variation of turbojet engine performance with engine speed. Flight Mach number, 0.25.

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(g) Exhaust-nozzle-outlet total temperature. Figure 5. - Concluded. Effect of altitude on variation of turbojet engine performance with engine speed. Flight Mach number, 0.25.

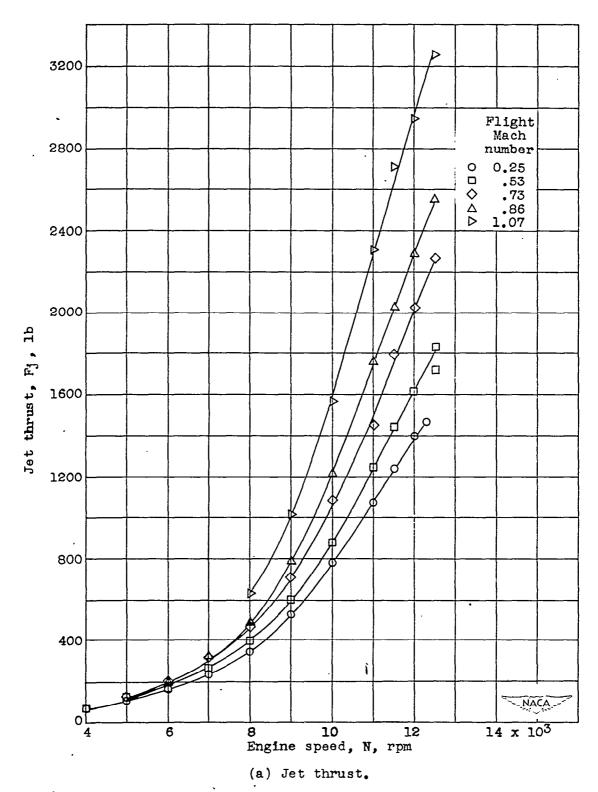


Figure 6. - Effect of flight Mach number on variation of turbojet engine performance with engine speed. Altitude, 25,000 feet.

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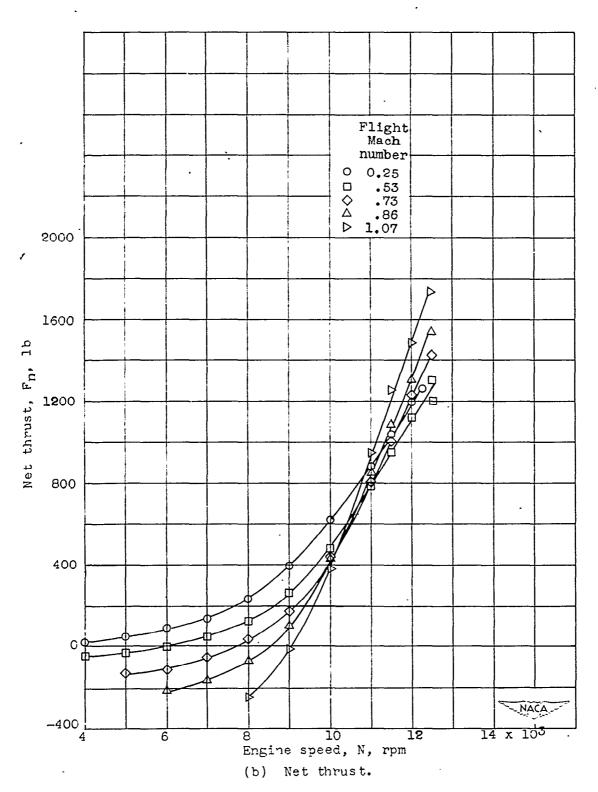


Figure 6. - Continued. Effect of flight Mach number on variation of turbojet engine performance with engine speed. Altitude, 25,000 feet.

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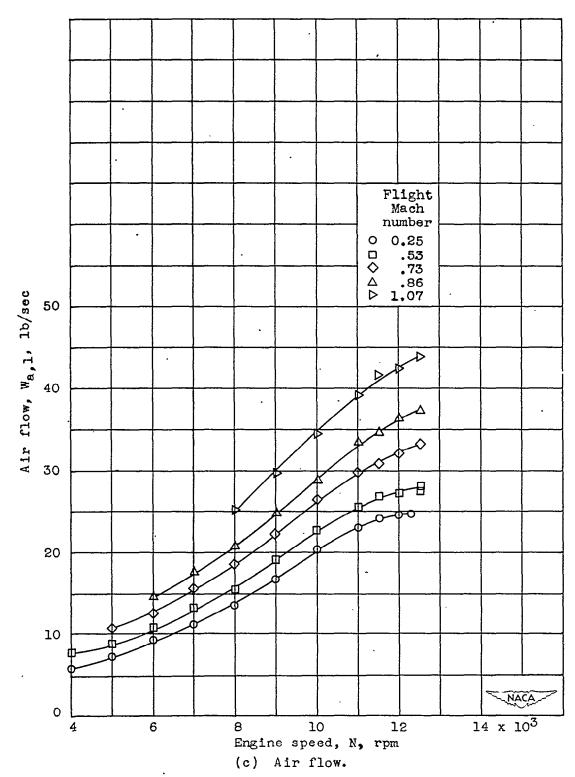


Figure 6. - Continued. Effect of flight Mach number on variation of turbojet engine performance with engine speed. Altitude, 25,000 feet.

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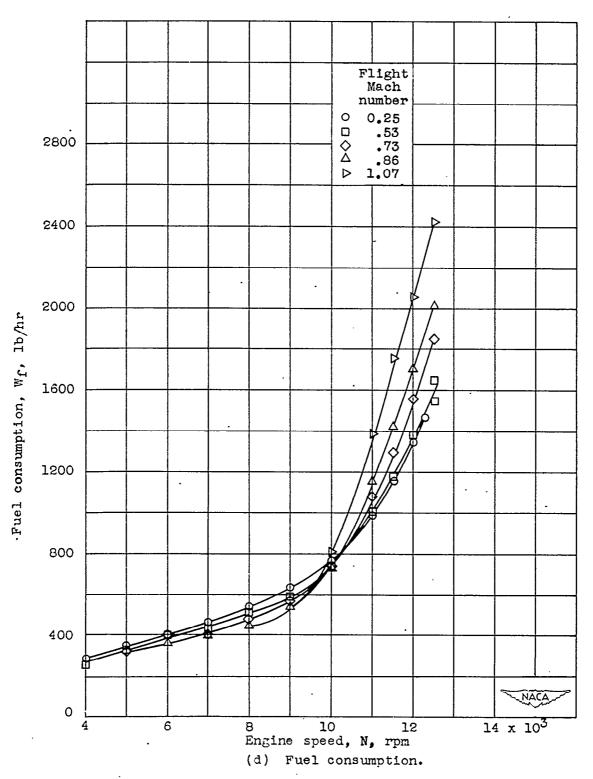
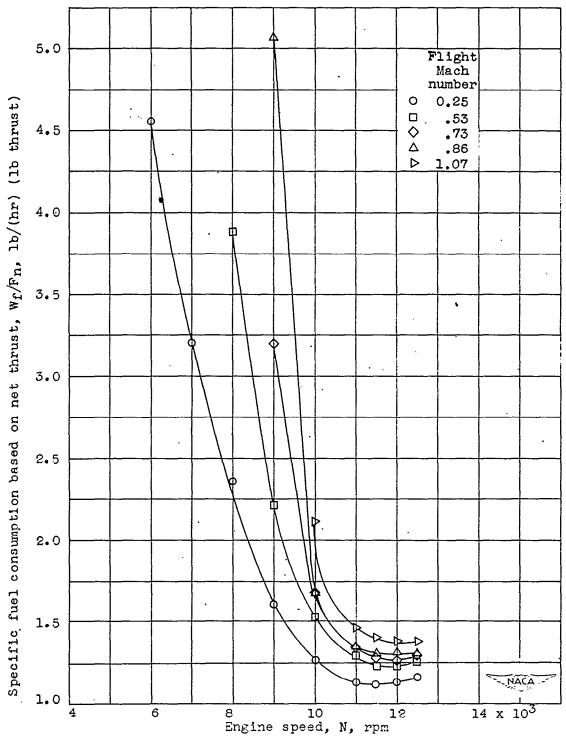


Figure 6. - Continued. Effect of flight Mach number on variation of turbojet engine performance with engine speed. Altitude, 25,000 feet.



(e) Specific fuel consumption based on net thrust.

Figure 6. - Continued. Effect of flight Mach number on variation of turbojet engine performance with engine speed. Altitude, 25,000 feet.

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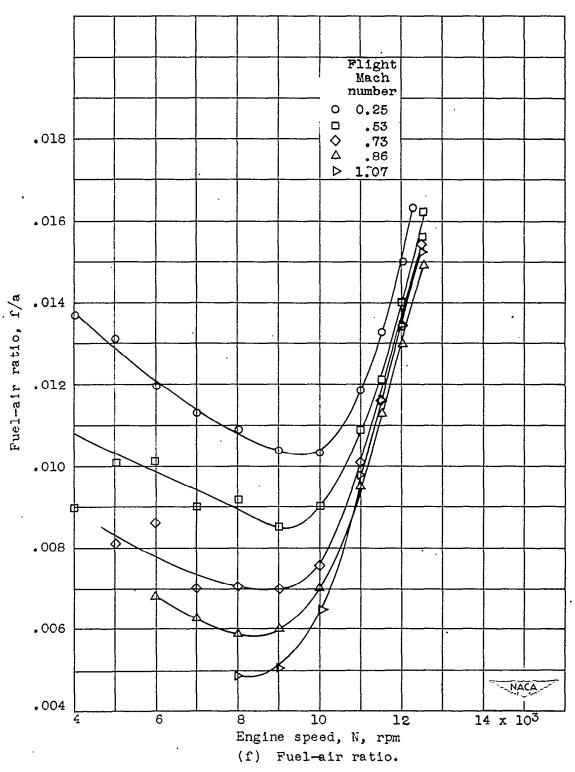
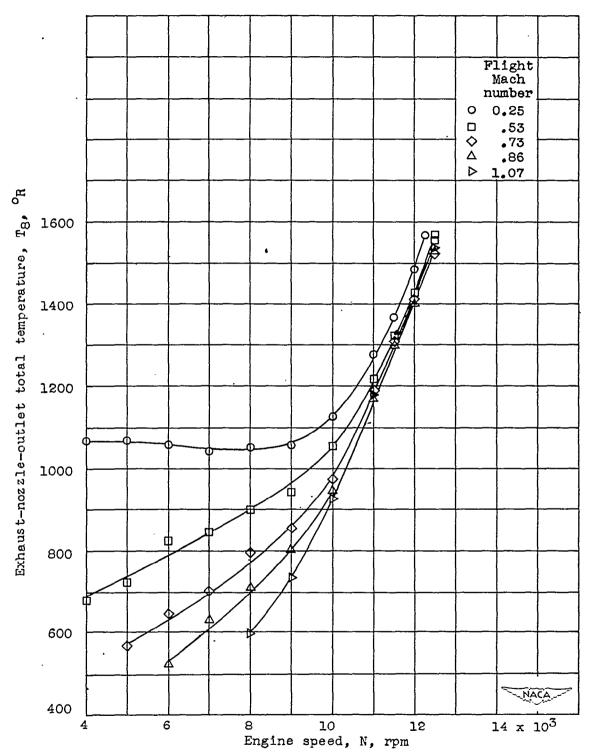


Figure 6. - Continued. Effect of flight Mach number on variation of turbojet engine performance with engine speed.
Altitude, 25,000 feet.

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(g) Exhaust-nozzle-outlet total temperature.

Figure 6. - Concluded. Effect of flight Mach number on variation of turbojet engine performance with engine speed. Altitude, 25,000 feet.

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Figure 7. - Effect of altitude on variation of generalized turbojet engine performance with corrected engine speed. Flight Mach number, 0.25.

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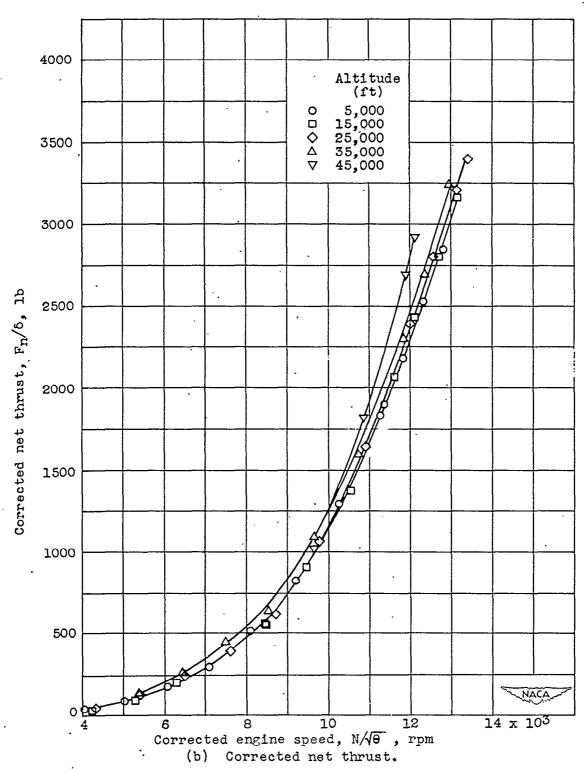


Figure 7. - Continued. Effect of altitude on variation of generalized turbojet engine performance with corrected engine speed. Flight Mach number, 0.25.

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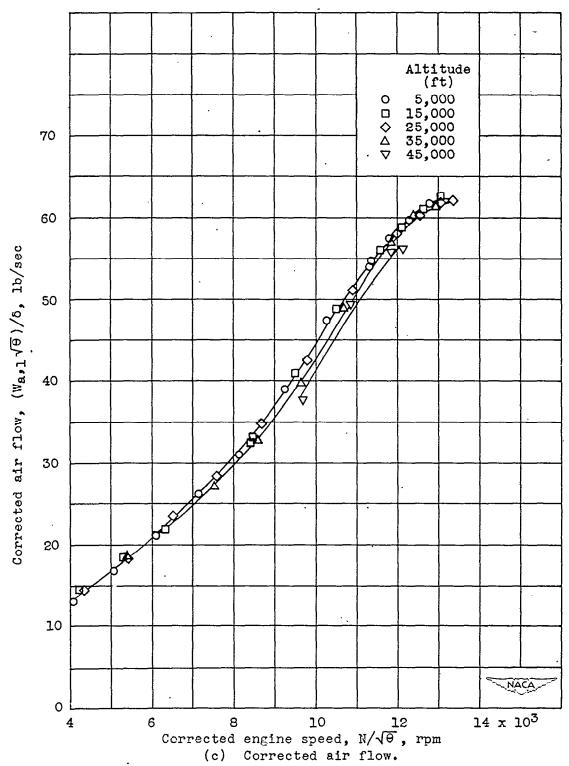


Figure 7. - Continued. Effect of altitude on variation of generalized turbojet engine performance with corrected engine speed. Flight Mach number, 0.25.

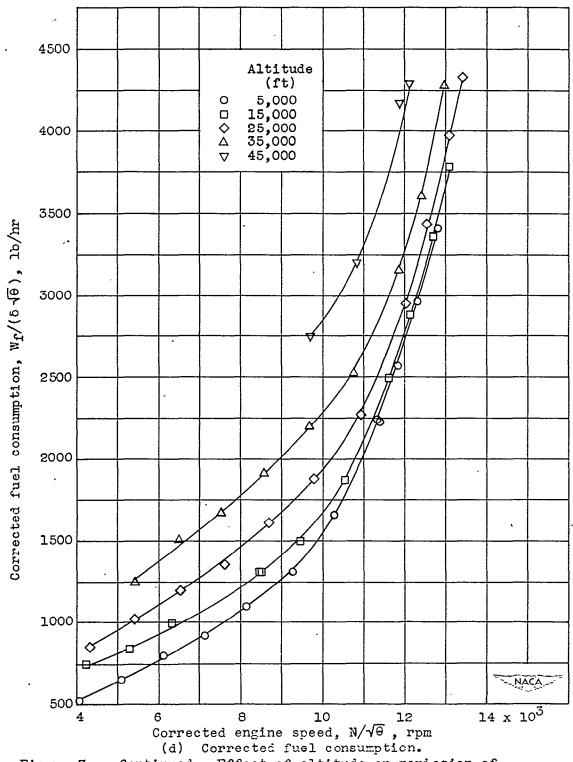
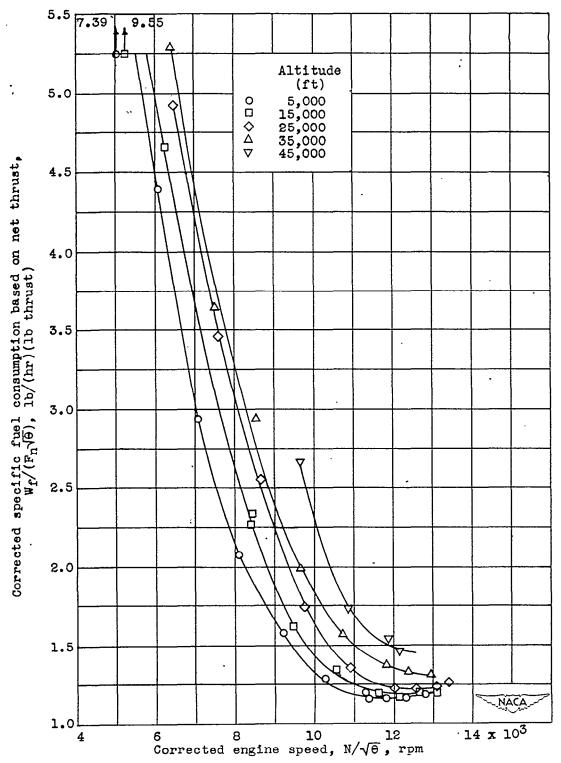


Figure 7. - Continued. Effect of altitude on variation of generalized turbojet engine performance with corrected engine speed. Flight Mach number, 0.25.

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(e) Corrected specific fuel consumption based on net thrust. Figure 7. - Continued. Effect of altitude on variation of generalized turbojet engine performance with corrected engine speed. Flight Mach number, 0.25.

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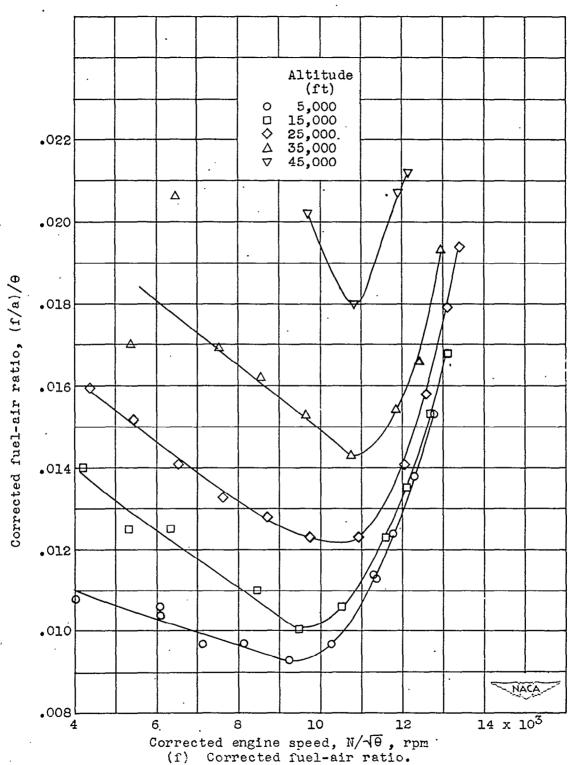
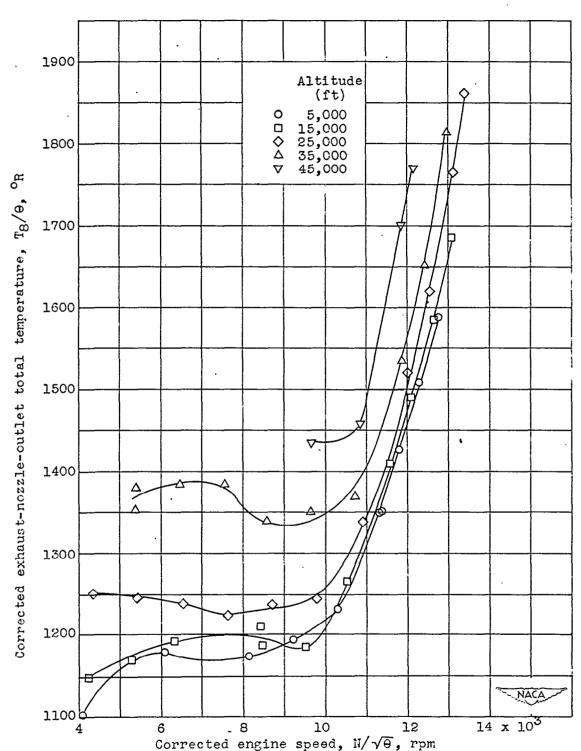


Figure 7. - Continued. Effect of altitude on variation of generalized turbojet engine performance with corrected engine speed. Flight Mach number, 0.25.

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(g) Corrected exhaust-nozzle-outlet total temperature.

Figure 7. - Concluded. Effect of altitude on variation of generalized turbojet engine performance with corrected engine speed. Flight Mach number, 0.25.

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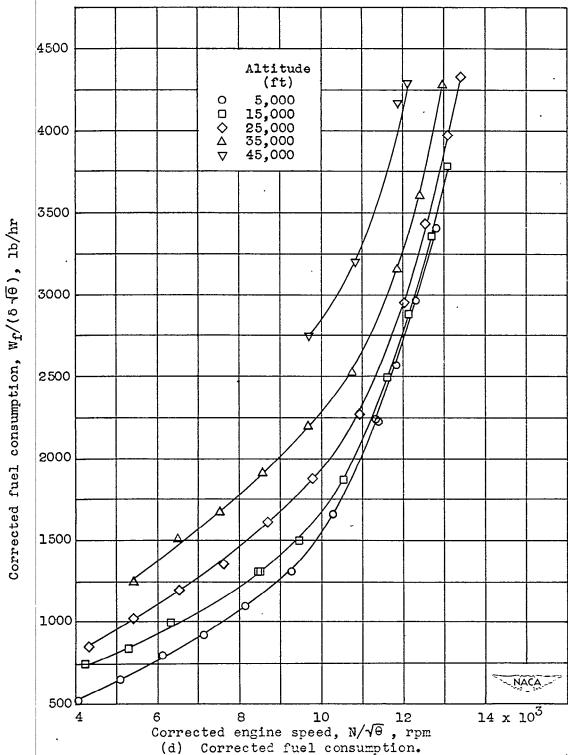
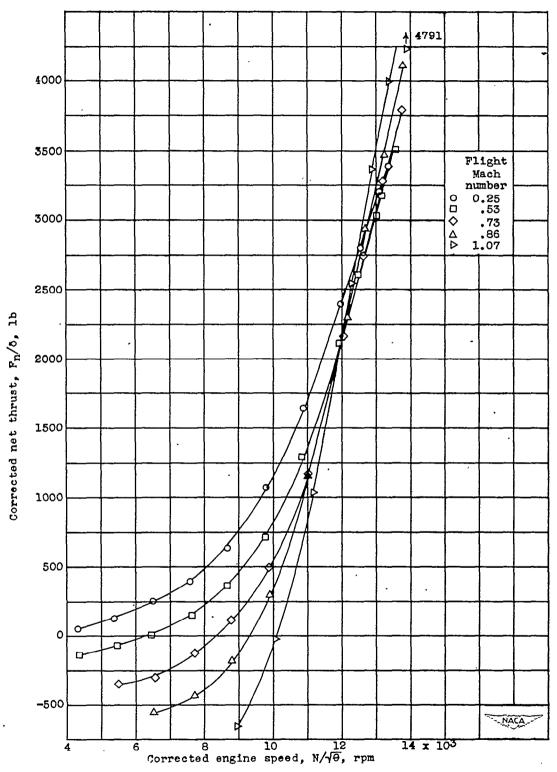


Figure 7. - Continued. Effect of altitude on variation of generalized turbojet engine performance with corrected engine speed. Flight Mach number, 0.25.

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(b) Corrected net thrust.

Figure 8. - Continued. Effect of flight Mach number on variation of generalized turbojet engine performance with corrected engine speed. Altitude, 25,000 feet.

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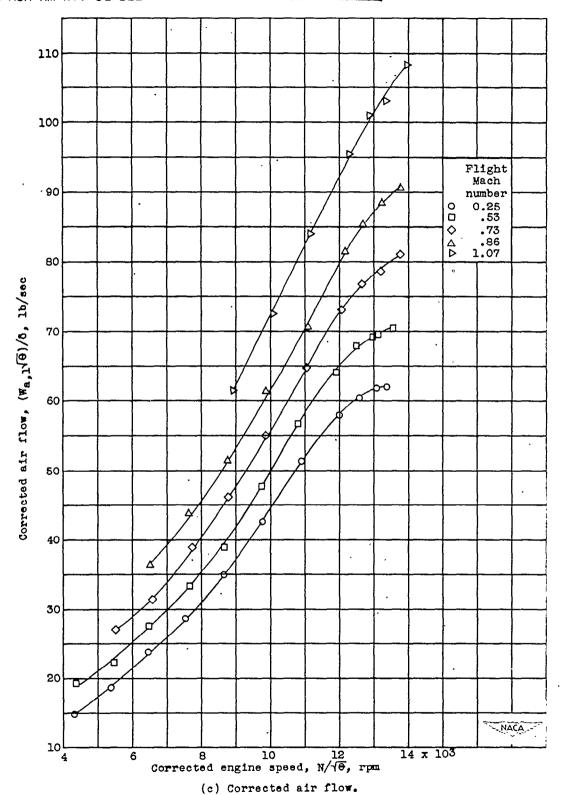
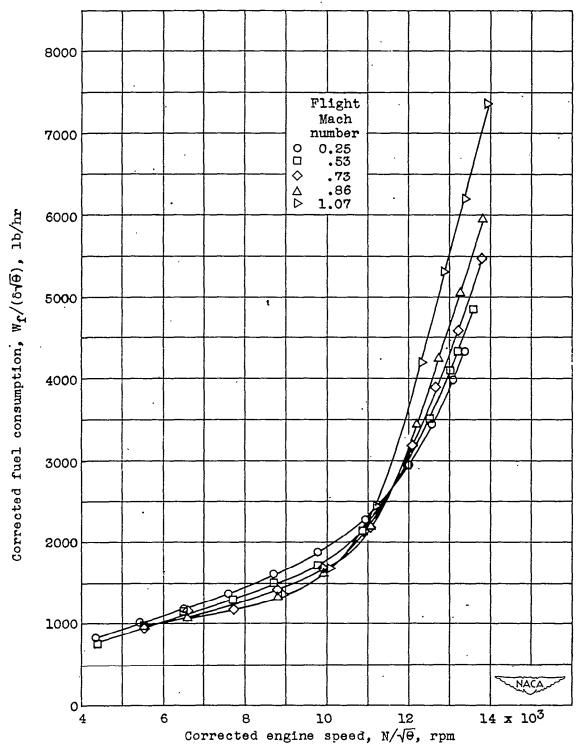


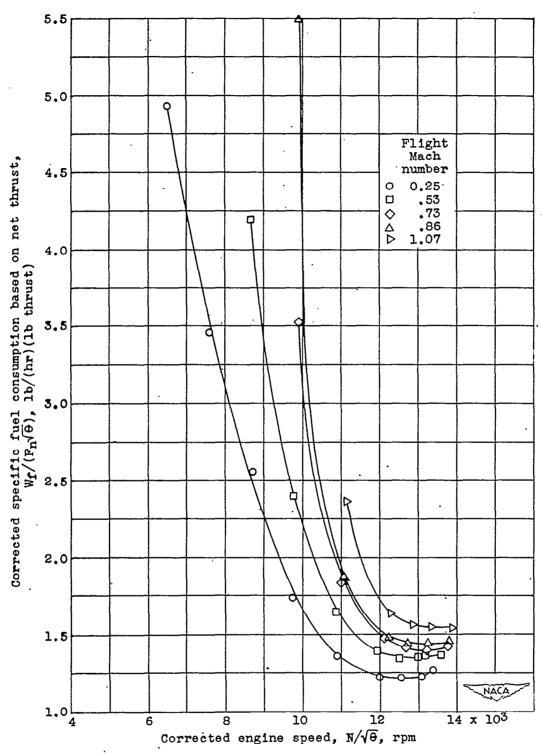
Figure 8. - Continued. Effect of flight Mach number on variation of generalized turbojet engine performance with corrected engine speed. Altitude, 25.000 feet.

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(d) Corrected fuel consumption.

Figure 8. - Continued. Effect of flight Mach number on variation of generalized turbojet engine performance with corrected engine speed. Altitude, 25,000 feet.



(e) Corrected specific fuel consumption based on net thrust.

Figure 8. - Continued. Effect of flight Mach number on variation of generalized turbojet engine performance with corrected engine speed. Altitude, 25,000 feet.

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-- NACA

 $14 \times 10^{3}$ 

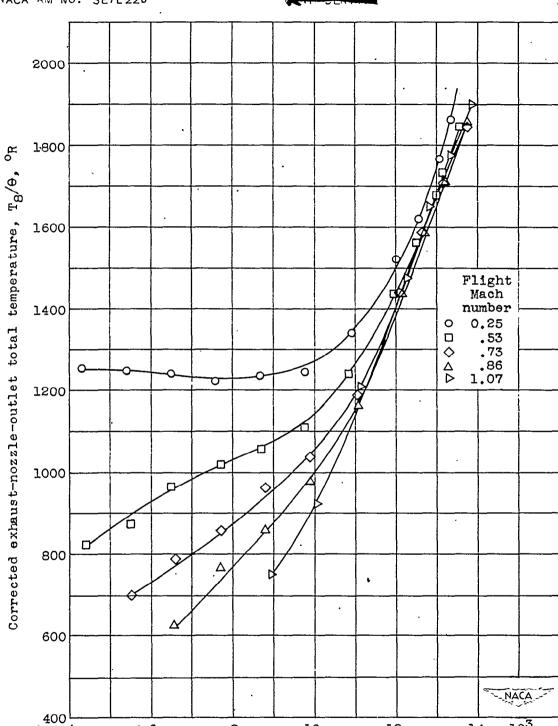
Corrected fuel-air ratio, (f/a)/0

.006

(f) Corrected fuel-air ratio.

10 Corrected engine speed,  $N\sqrt{\theta}$ , rpm

Figure 8. - Continued. Effect of flight Mach number on variation of generalized turbojet engine performance with corrected engine speed. Altitude, 25,000 feet.



Corrected engine speed,  $N/\sqrt{\theta}$ , rpm (g) Corrected exhaust-nozzle-outlet total temperature.

8

10

12

<sup>-</sup> 6

Figure 8. - Concluded. Effect of flight Mach number on variation of generalized turbojet engine performance with corrected engine speed. Altitude, 25,000 feet.

 $14 \times 10^{3}$ 

